

| COMPANY NAME | | Calculation No. | | |
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| | | CALCULATION NUMBER | | |
| CALCULATION SHEET | | Project No. | | |
| onlinestructuraldesign.com | | PROJECT NUMBER | | |
| Project Title: | Project Name | Calc. By | Date | Rev. |
| | | Author | today | 0 |
| Subject/Feature: | Bolt Preloading Force - Classes 8.8 and 10.9 (Eurocode 3) | Checked By | Date | |
| | | Checker | today | |
| Bolt preloading force - Classes 8.8 and 10.9 (Eurocode 3) | | per EN 1993-1-8 and EN 1090-2 | | |
| Input | Output | | | |
| Bolt type, class and diameter | Bolt design preload (tension in bolt) | | | |
| Partial factors for steel bolts | Bolt torque reference value for tightening (slip resistant connection) | | | |
| | Bolt torque value for tightening (non-slip resistant connection) | | | |
| Bolts Type | 16 | bolt diameter - d | | |
| $A_s =$ | 157 mm ² | bolt effective area in threaded region | | |
| Bolt class | 10.9 | per EN 1993-1-8 Section 3 Table 3.1 | | |
| Bolt yield strength | $f_{yb} = 900$ N/mm ² | Bolt ultimate tensile strength | $f_{ub} = 1000$ N/mm ² | |
| | | bolt classes recommended by the Eurocode; The National Annex may exclude certain bolt classes. | | |
| Partial factor for steel bolts | $\gamma_{M2} = 1.25$ | per EN 1993-1-8 Section 2 Table 2.1 | | |
| | $\gamma_{M7} = 1.1$ | partial safety factors recommended by the Eurocode; Numerical values for safety factors may be defined in the National Annex | | |
| Bolt design strength | $f_{yd} = f_y / \gamma_{M2}$ | | | |
| | $f_{yd} = 818.2$ N/mm ² | | | |
| Bolt design tension resistance | $F_{t,Rd} = f_{yd} * A_s$ | | | |
| | $F_{t,Rd} = 128.45$ kN | | | |
| Bolt design preload | per EN 1993-1-8 Section 3.6.1 Formula (3.1) | | | |
| | $F_{p,Cd} = 0.7 * f_{ub} * A_s / \gamma_{M7}$ | for preloaded bolts in accordance with 3.1.2(1) (i.e. only bolt assemblies of classes 8.8 and 10.9) | | |
| | $F_{p,Cd} = 99.91$ kN | | | |
| Torque reference values for bolt tightening | per EN 1090-2 Section 8.5.2 Paragraph a) - 1) and 2) | | | |
| | $M_r = k_m * d * F_{p,Cd}$ | k-class (K1 or K2) and k_m value declared by the fastener manufacturer | | |
| | $k_m = 0.2$ | (normally $k=0.2$ for typical steel, $k=0.2$ for zinc-plated, $k=0.18$ for lubricated, $k=0.16$ for cadmium-plated) | | |
| | $M_r = 319.7$ kN*m | torque value when the connection is slip resistant | | |
| | $50 \% * F_{p,Cd} = 49.95$ kN | per EN 1993-1-8 Section 3.4.2, Note: If preload is not explicitly used in the design calculations for slip resistances but is required for execution purposes or as a quality measure (e.g. for durability) then the level of preload can be specified in the National Annex. | | |
| Torque value when there is no slip resistance specified in the design | value for 50 % of the bolt preload capacity | | | |
| | $M_{r(non\ slip)} = 159.9$ kN*m | | | |
| References: | | | | |
| EN 1090-2:2008 Execution of steel structures and aluminium structures - Part 2: Technical requirements for steel structures | | | | |
| EN 1993-1-8:2005 - Eurocode 3: Design of steel structures - Part 1-8: Design of joints | | | | |